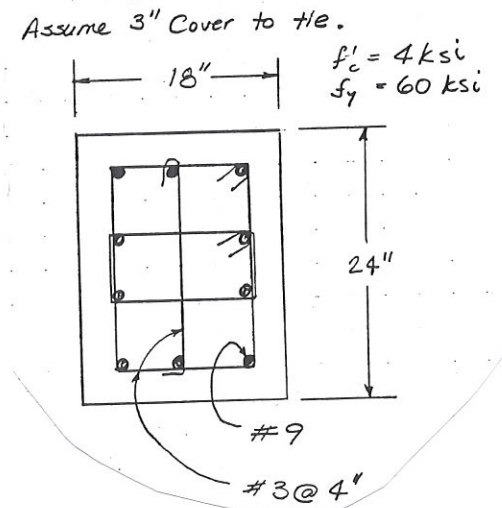


Advanced Concrete Member Behavior  
 CEE6301-01

Problem 1 : [Total 50 points]

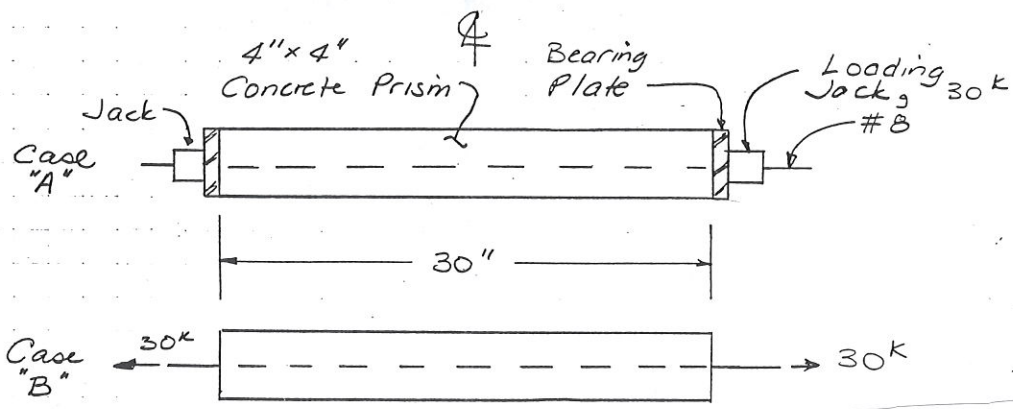
- (A) For the column cross section shown below, calculate the peak stress capacity of the confined core. Cylinder strength test of 4000 psi achieved. [25 points]  
 (B) Describe expected post-spalling behavior under axial load of a ten foot long column with the cross-section shown below. [25 points]



Problem 2 : [Total 50 points]

Shown below are two concrete prism with embedded #8 longitudinal bar bonded to the concrete.  $f'_c = 4000 \text{ psi}$  and  $f_y = 60,000 \text{ psi}$ .

- (A) Two jacks pull the #8 bar, reacting against bearing plates that are exposed to the prism. Calculate the bar slip from concrete at one end when tension of 30 kips is applied. Case "A" [25 points]  
 (B) The bars are pulled with same 30 kip force with no reaction on concrete. Calculate the slip from concrete at one end. Case "B" [25 points]



Good Luck!

$$\bar{a} = \frac{f_t A_c}{\pi d_o^2} \times 1.5$$

$$f_c = 2 \left( \frac{E_c}{E_o} \right) \left( 1 - \frac{1}{2} \left( \frac{E_c}{E_o} \right) \right) f_c'$$

$$\sigma_a = (\sigma_1 + \sigma_2 + \sigma_3) / 3$$

$$\sigma = \left[ \frac{\sum x_i^2 - (\sum x_i)^2 / n}{(n-1)} \right]^{1/2}$$

$$l_s = \frac{1860}{\sqrt{f_c'}} d_b \geq 20 d_b$$

$$f_r = \frac{\pi^2 E}{(k l / r)^2}$$

$$r = d_o / 4$$

$$\rho_o = 0.85 \beta_1 \frac{f_c'}{f_y} \frac{87000}{87000 + f_y}$$

$$\bar{\sigma}_a = \frac{1}{\sqrt{15}} \left[ (\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \right]^{1/2} \quad \therefore k = k_{tr} + c$$

$$f_{cr} = f_c' + t \sigma$$

$$\rho_s = 0.45 \left( \frac{A_g}{A_c} - 1 \right) \frac{f_c'}{f_y}$$

$$A_{sh} \geq 0.09 S_h \frac{f_c'}{f_y}$$

$$z = \frac{0.5}{\frac{3 + 0.002 f_c'}{f_c' - 10000}} + \frac{3}{4 \rho_s} \sqrt{\frac{b}{s}} - 0.002$$

$$l_d = \frac{5500 A_b}{\phi k \sqrt{f_c'}}$$

$$k_{tr} = \frac{A_{tr} f_y}{1500 s}$$

$$\rho_s \geq 0.12 \frac{f_c'}{f_y}$$

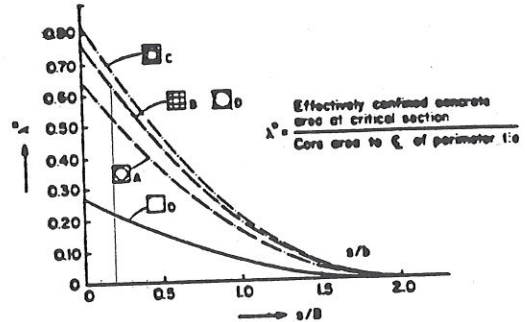


FIG. 7.—Effectively Confined Concrete Area as a Function of Tie Spacing and Core Size for Various Square Steel Configurations

$$A_{sh} = 0.3 \left( \frac{A_g}{A_c} - 1 \right) \frac{f_c'}{f_y} S_h$$

$$f_{cmax} = f_c' + 4.1 f_r$$

$$f_c = f_{cmax} \left[ 1 - z (E_c - E_s k) \right]$$

bar#	$d_b$ (in)	$A_b$ (in <sup>2</sup> )
3	3/8	0.11
4	4/8	0.20
5	5/8	0.31
6	6/8	0.44
7	7/8	0.60
8	1	0.79
9	1.12	1.00
11	1.44	1.56